

# EMITTANCE EXCHANGE

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- ❖ Introduction
- ❖ Physical Analysis
- ❖ Beam Line Design
- ❖ Applications
- ❖ Summary

# INTRODUCTION

- ❖ Different applications present different requirements on the quality of the particle beam.
- ❖ Many beam applications have stringent emittance requirements for successful operation, and are not always compatible with the beam characteristics of available accelerators.

$$\varepsilon_{n,x} \varepsilon_{n,y} \varepsilon_{n,z}$$



$$\varepsilon_{n,x} : \varepsilon_{n,y} : \varepsilon_{n,z}$$



- ❖ In this case it will be very useful to exchange the emittances between two different dimensions to make all of the requirements about emittance are met.

- ❖ Uncoupled beam sigma matrix:

$$\sigma_0 = \begin{pmatrix} \sigma_x & \mathbf{0} \\ \mathbf{0} & \sigma_z \end{pmatrix} = \begin{pmatrix} \varepsilon_{x0}\beta_x & -\varepsilon_{x0}\alpha_x & 0 & 0 \\ -\varepsilon_{x0}\alpha_x & \varepsilon_{x0}\gamma_x & 0 & 0 \\ 0 & 0 & \varepsilon_{z0}\beta_z & -\varepsilon_{z0}\alpha_z \\ 0 & 0 & -\varepsilon_{z0}\alpha_z & \varepsilon_{z0}\gamma_z \end{pmatrix}$$

- ❖ Through the transfer matrix:  $\sigma = \mathbf{R}\sigma_0\mathbf{R}^T$

- ❖ The transfer matrix should be coupled to achieve the emittance exchange.

- ❖ Coupled component: dipole, dogleg, chicane, etc.

- ❖ The 4\*4 matrix is constructed from four 2\*2 blocks,

$$\mathbf{R} = \begin{pmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{pmatrix}$$

- ❖ The beam matrix can be expressed as:

$$\boldsymbol{\sigma} = \begin{pmatrix} \mathbf{A}\boldsymbol{\sigma}_x\mathbf{A}^T + \mathbf{B}\boldsymbol{\sigma}_z\mathbf{B}^T & \mathbf{A}\boldsymbol{\sigma}_x\mathbf{C}^T + \mathbf{B}\boldsymbol{\sigma}_z\mathbf{D}^T \\ \mathbf{C}\boldsymbol{\sigma}_x\mathbf{A}^T + \mathbf{D}\boldsymbol{\sigma}_z\mathbf{B}^T & \mathbf{C}\boldsymbol{\sigma}_x\mathbf{C}^T + \mathbf{D}\boldsymbol{\sigma}_z\mathbf{D}^T \end{pmatrix}$$

- ❖ Final emittance after matrix transformation

$$\varepsilon_x^2 = \left| \mathbf{A}\boldsymbol{\sigma}_x\mathbf{A}^T + \mathbf{B}\boldsymbol{\sigma}_z\mathbf{B}^T \right|$$

$$\varepsilon_z^2 = \left| \mathbf{C}\boldsymbol{\sigma}_x\mathbf{C}^T + \mathbf{D}\boldsymbol{\sigma}_z\mathbf{D}^T \right|$$

$$\varepsilon_x^2 = |\mathbf{A}|^2 \varepsilon_{x0}^2 + (1 - |\mathbf{A}|)^2 \varepsilon_{z0}^2 + \varepsilon_{x0} \varepsilon_{z0} \lambda^2$$

$$\varepsilon_z^2 = (1 - |\mathbf{A}|)^2 \varepsilon_{x0}^2 + |\mathbf{A}|^2 \varepsilon_{z0}^2 + \varepsilon_{x0} \varepsilon_{z0} \lambda^2$$

$$\begin{aligned} \sigma_x = \varepsilon_{x0} \mathbf{Q}_x \mathbf{Q}_x^T & \quad \mathbf{Q}_x = \frac{1}{\sqrt{\beta_x}} \begin{pmatrix} \beta_x & 0 \\ -\alpha_x & 1 \end{pmatrix} & \quad \mathbf{U} = \mathbf{Q}_x^{-1} \mathbf{A}^a \mathbf{B} \mathbf{Q}_z \\ \sigma_z = \varepsilon_{z0} \mathbf{Q}_z \mathbf{Q}_z^T & \quad \mathbf{Q}_z = \frac{1}{\sqrt{\beta_z}} \begin{pmatrix} \beta_z & 0 \\ -\alpha_z & 1 \end{pmatrix} & \quad \mathbf{V} = \mathbf{Q}_z^{-1} \mathbf{C}^a \mathbf{D} \mathbf{Q}_z \end{aligned} \quad \text{tr}\{\mathbf{U}\mathbf{U}^T\} = \text{tr}\{\mathbf{V}\mathbf{V}^T\} = \lambda^2 \geq 0$$

❖ To achieve  $\varepsilon_x = \varepsilon_{z0}$  and  $\varepsilon_z = \varepsilon_{x0}$

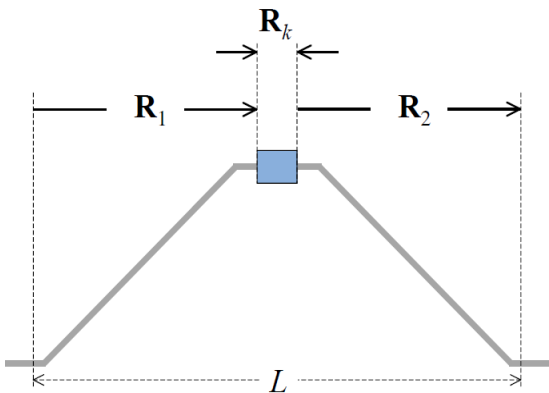
$$|\mathbf{A}| = 0$$

$$\lambda^2 = 0 \quad \longrightarrow \quad A_{i,j} = D_{i,j} = 0$$

$$\mathbf{R} = \begin{pmatrix} 0 & 0 & * & * \\ 0 & 0 & * & * \\ * & * & 0 & 0 \\ * & * & 0 & 0 \end{pmatrix}$$

# BEAMLINE DESIGN

1



$$\mathbf{R}_k = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & k & 0 \\ 0 & 0 & 1 & 0 \\ k & 0 & 0 & 1 \end{pmatrix}$$

$$\mathbf{R}_1 = \begin{pmatrix} 1 & L/2 & 0 & \eta \\ 0 & 1 & 0 & 0 \\ 0 & \eta & 1 & \xi/2 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$k \equiv \frac{eV_0}{aE}$$

$\eta$  and  $\xi$  are dispersion and momentum compaction Factor respectively

$$\mathbf{R}_2 = \begin{pmatrix} 1 & L/2 & 0 & -\eta \\ 0 & 1 & 0 & 0 \\ 0 & -\eta & 1 & \xi/2 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\mathbf{R} = \begin{pmatrix} 1 - \eta k & L & kL/2 & k\left(\frac{\xi L}{4} - \eta^2\right) \\ 0 & 1 + \eta k & k & k\xi/2 \\ k\xi/2 & k\left(\frac{\xi L}{4} - \eta^2\right) & 1 - \eta k & \xi \\ k & kL/2 & 0 & 1 + \eta k \end{pmatrix}$$



$$\mathbf{R} = \begin{pmatrix} 0 & 0 & * & * \\ 0 & 0 & * & * \\ * & * & 0 & 0 \\ * & * & 0 & 0 \end{pmatrix}$$

❖ Considering a simple case:  $1 - \eta k = 0$   $\longrightarrow$   $|\mathbf{A}| = |\mathbf{D}| = 0$   $|\mathbf{B}| = |\mathbf{C}| = 1$

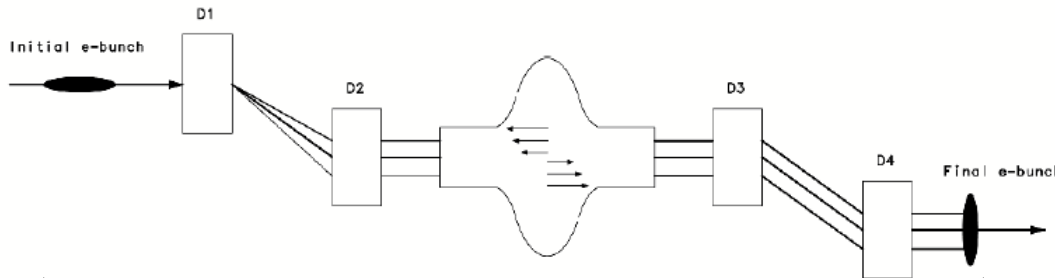
$$\varepsilon_x = \sqrt{\varepsilon_{z0}^2 + 4\sigma_{x'}^2 \sigma_\delta^2 \eta^2}$$

$$\varepsilon_z = \sqrt{\varepsilon_{x0}^2 + 4\sigma_{x'}^2 \sigma_\delta^2 \eta^2}$$

Reference: Cornacchia M, Emma P. PRST, 2002, 5(8): 084001.

# BEAMLINE DESIGN

## 2 An improved beamline



$$\mathbf{R}_k = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & k & 0 \\ 0 & 0 & 1 & 0 \\ k & 0 & 0 & 1 \end{pmatrix}$$

$$\mathbf{R} = \begin{pmatrix} 1 + \eta k & L(1 + \eta k) & kL/2 & k\left(\frac{\xi L}{4} + \eta^2\right) + 2\eta \\ 0 & 1 + \eta k & k & k\xi/2 \\ k\xi/2 & k\left(\frac{\xi L}{4} + \eta^2\right) + 2\eta & 1 + \eta k & \xi + \eta k\xi \\ k & kL/2 & 0 & 1 + \eta k \end{pmatrix}$$

$$\mathbf{R}_2 = \mathbf{R}_1 = \begin{pmatrix} 1 & L/2 & 0 & \eta \\ 0 & 1 & 0 & 0 \\ 0 & \eta & 1 & \xi/2 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

❖ Considering the case  $1 + \eta k = 0$

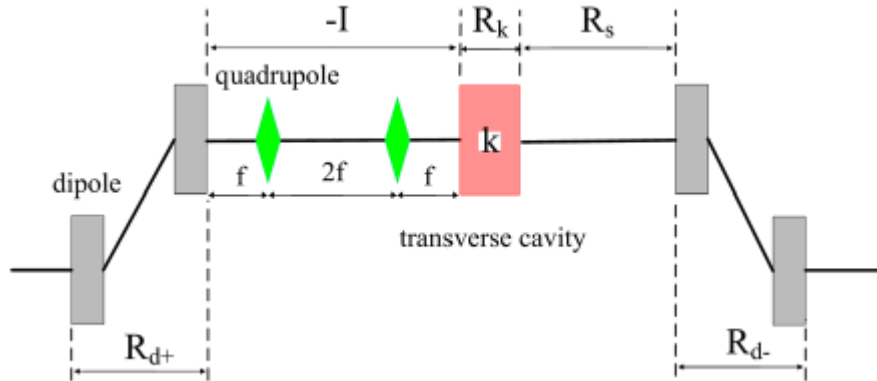
$$\mathbf{R} = \begin{pmatrix} 0 & 0 & kL/2 & \frac{k\xi L}{4} + \eta \\ 0 & 0 & k & k\xi/2 \\ k\xi/2 & \frac{k\xi L}{4} + \eta & 0 & 0 \\ k & kL/2 & 0 & 0 \end{pmatrix}$$



$$\mathbf{R} = \begin{pmatrix} 0 & 0 & * & * \\ 0 & 0 & * & * \\ * & * & 0 & 0 \\ * & * & 0 & 0 \end{pmatrix}$$



## 3 Another improved beamline

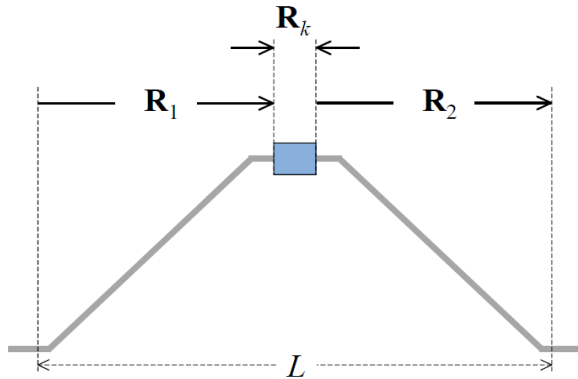


❖ Considering the case  $\eta k = 1$

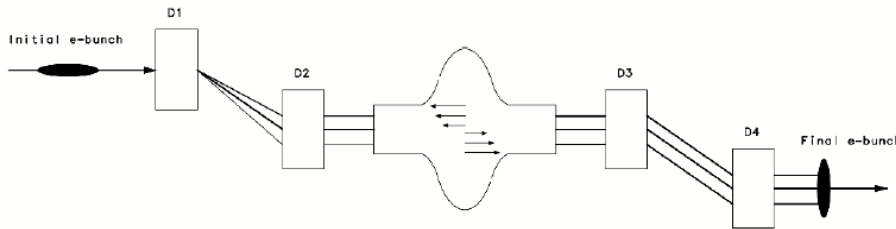
$$R_c = \begin{bmatrix} 0 & 0 & k(L+S) & k\xi(L+S) - \eta \\ 0 & 0 & k & k\xi \\ -k\xi & \eta - kL\xi & 0 & 0 \\ -k & -kL & 0 & 0 \end{bmatrix} \longleftrightarrow \mathbf{R} = \begin{pmatrix} 0 & 0 & * & * \\ 0 & 0 & * & * \\ * & * & 0 & 0 \\ * & * & 0 & 0 \end{pmatrix}$$

# BEAMLINE DESIGN

- Comparison of different beamlines

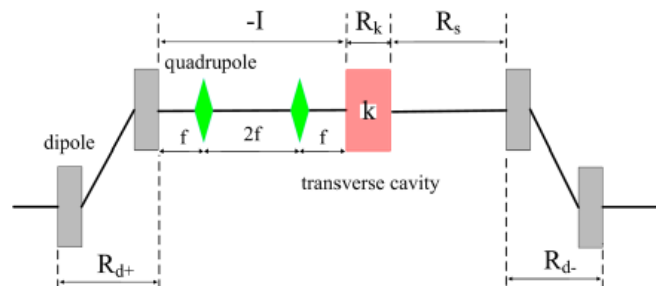


incomplete exchange



complete exchange

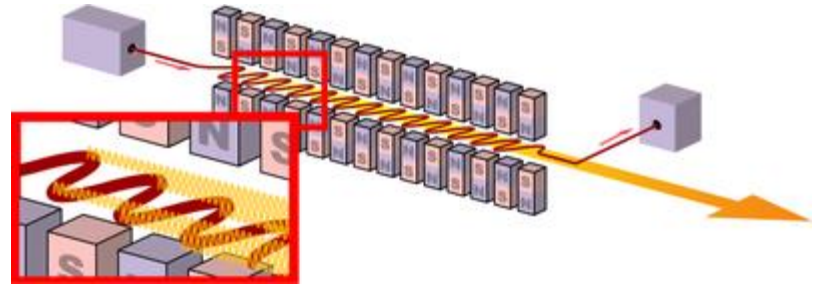
Experimental verification  
offset of the beam trajectory



complete exchange  
no offset of the beam trajectory  
paperwork

## ✓ Emittance Exchange

- ❑ **To achieve lower transverse emittance in FELs.**

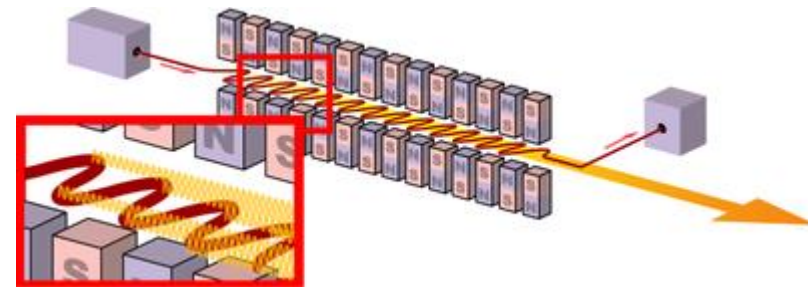


- ❑ **Phase space exchange (generating tunable subpicosecond electron-bunch-train).**

# APPLICATIONS

- To achieve lower transverse emittance in FELs

Transverse emittance  $\varepsilon_{n,x} \leq \lambda\gamma / 4\pi$



$$(\varepsilon_x, \varepsilon_y, \varepsilon_z) = (1, 1, 0.1)$$

↓ ↓

$$(10, 0.1, 0.1)$$

round to flat beam transformation

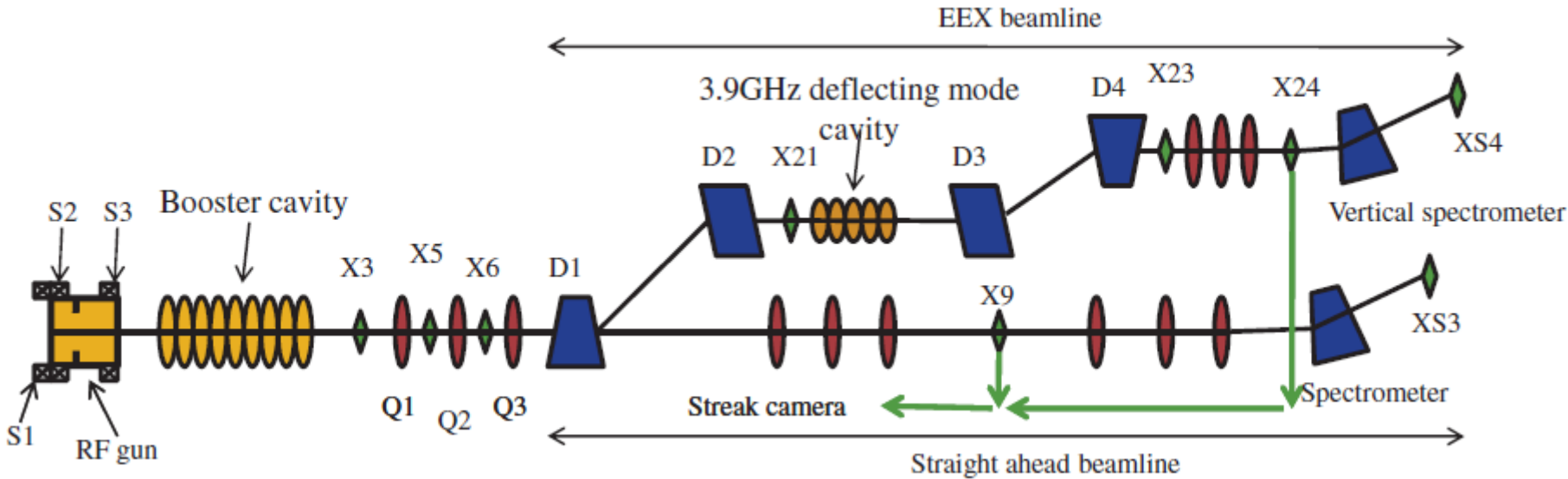
↙ ↘

$$(0.1, 0.1, 10)$$

longitudinal to transverse emittance exchange

# APPLICATIONS

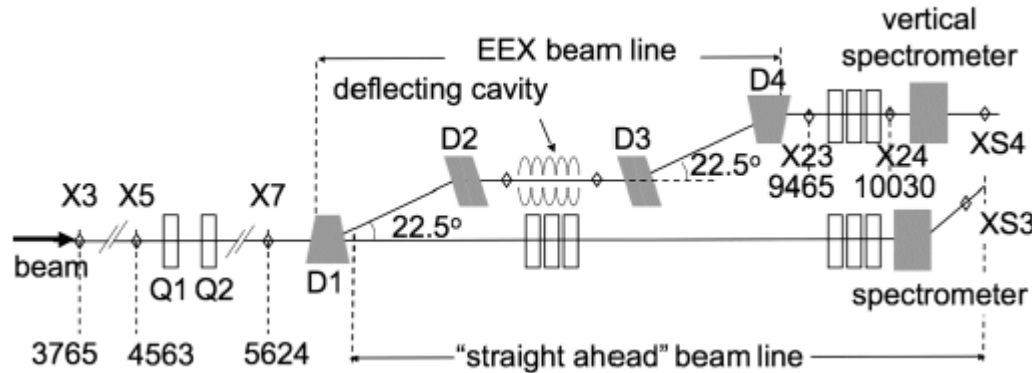
- To achieve lower transverse emittance in FELs



	Simulated		Measured	
	In	Out	In	Out
$\epsilon_{nx}$	2.9	13.2	$2.9 \pm 0.1$	$11.3 \pm 1.1$
$\epsilon_{ny}$	2.4	2.4	$2.4 \pm 0.1$	$2.9 \pm 0.5$
$\epsilon_{nz}$	13.1	3.2	$13.1 \pm 1.3$	$3.1 \pm 0.3$

Reference: Ruan J, Johnson A S, Lumpkin A H, et al. PRL, 2011, 106(24): 244801.

## Tunable Subpicosecond Electron-Bunch-Train Generation

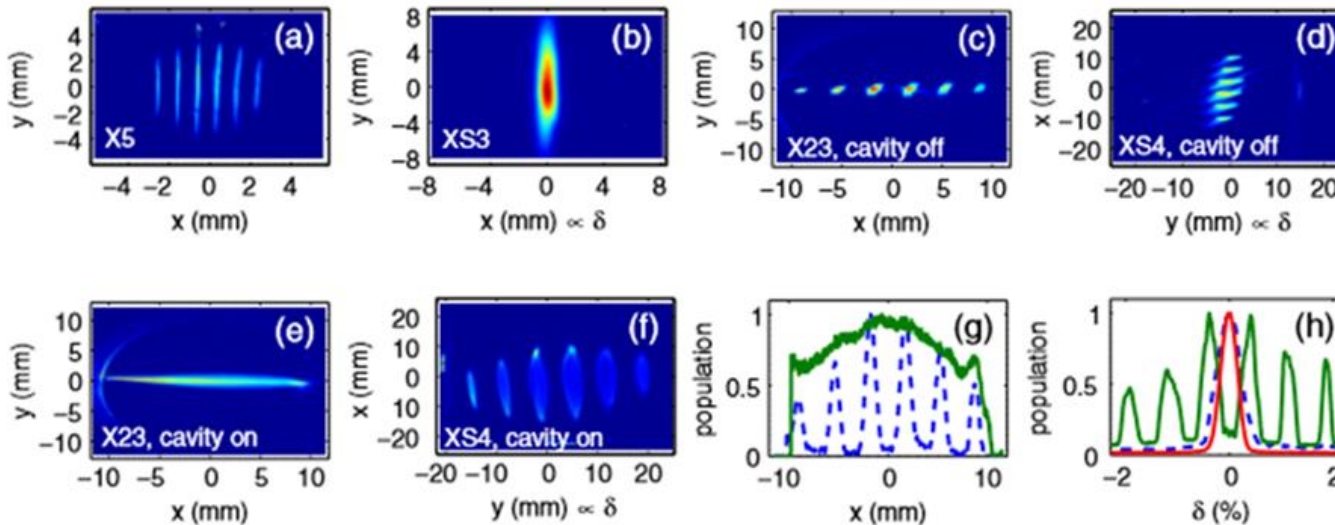


Result:

Bunch spacing: 1.2ps  
rms duration for each bunch: <300fs

Bunch charge:

slits out: 550pC  
slits in: ~15pC



- 1、 generation of super-radiant radiation
- 2、 excitation of wakefields in beam-driven acceleration

- ❖ EEX is expensive due to RF and thermal considerations
- ❖ Modern photoinjectors produce low emittance beam (no need for EEX)

## ❖ The physical principle

Emittance exchange condition:

$$\mathbf{R} = \begin{pmatrix} 0 & 0 & * & * \\ 0 & 0 & * & * \\ * & * & 0 & 0 \\ * & * & 0 & 0 \end{pmatrix}$$

## ❖ Three different beamlines

Advantages and disadvantages

## ❖ Applications

1 To achieve lower transverse emittance  
in FELs

2 Phase space exchange to generate  
tunable subpicosecond electron-  
bunch-train



# REFERENCES

- [1] Cornacchia M, Emma P. PRST, 2002, 5(8): 084001.
- [2] Emma P, Huang Z, Kim K J, et al. PRST, 2006, 9(10): 100702.
- [3] Xiang D, Chao A. PRST, 2011, 14(11): 114001.
- [4] Ruan J, Johnson A S, Lumpkin A H, et al. PRL, 2011, 106(24): 244801.
- [5] Sun Y E, Piot P, Johnson A, et al. PRL, 2010, 105(23): 234801.

**Thank you**

